## FEATURES

SNR = $\mathbf{7 5}$ dB, fiN 15 MHz, up to 105 MSPS
SNR = $\mathbf{7 2}$ dB, $\mathrm{f}_{\mathrm{IN}} \mathbf{2 0 0 ~ M H z , ~ u p ~ t o ~} \mathbf{1 0 5}$ MSPS
SFDR = 89 dBc , fin 70 MHz , up to 105 MSPS
100 dBFS multitone SFDR
IF sampling to $\mathbf{2 0 0} \mathbf{~ M H z}$
Sampling jitter: 0.1 ps
1.5 W power dissipation

Differential analog inputs
Pin compatible to AD6644
Twos complement digital output format
3.3 V CMOS compatible

Data-ready for output latching

## APPLICATIONS

Multichannel, multimode receivers
Base station infrastructures
AMPS, IS-136, CDMA, GSM, W-CDMA
Single channel digital receivers
Antenna array processing
Communications instrumentation
Radars, infrared imaging
Instrumentation

## GENERAL DESCRIPTION

The AD6645 is a high speed, high performance, monolithic 14-bit analog-to-digital converter (ADC). All necessary functions, including track-and-hold (T/H) and reference, are included on the chip to provide a complete conversion solution. The AD6645 provides CMOS-compatible digital outputs. It is the fourth
generation in a wideband ADC family, preceded by the AD9042 (12-bit, 41 MSPS), the AD6640 (12-bit, 65 MSPS, IF sampling), and the AD6644 (14-bit, 40 MSPS/65 MSPS).

Designed for multichannel, multimode receivers, the AD6645 is part of the Analog Devices, Inc., SoftCell ${ }^{\circ}$ transceiver chipset. The AD6645 maintains 100 dB multitone, spurious-free dynamic range (SFDR) through the second Nyquist band. This breakthrough performance eases the burden placed on multimode digital receivers (software radios) that are typically limited by the ADC. Noise performance is exceptional; typical signal-to-noise ratio (SNR) is 74.5 dB through the first Nyquist band.
The AD6645 is built on the Analog Devices extra fast complementary bipolar (XFCB) process and uses an innovative, multipass circuit architecture. Units are available in thermally enhanced 52-lead PowerQuad 4 (LQFP_PQ4) and 52-lead exposed pad (TQFP_EP) packages specified from $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ at 80 MSPS and $-10^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ at 105 MSPS.

## PRODUCT HIGHLIGHTS

1. IF Sampling. The AD6645 maintains outstanding ac performance up to input frequencies of 200 MHz , suitable for multicarrier 3 G wideband cellular IF sampling receivers.
2. Pin Compatibility. The ADC has the same footprint and pin layout as the AD6644 14-bit, 40 MSPS/65 MSPS ADC.
3. SFDR Performance and Oversampling. Multitone SFDR performance of 100 dBFS can reduce the requirements of high end RF components and allows the use of receive signal processors, such as the AD6620, AD6624/AD6624A, or AD6636.

## FUNCTIONAL BLOCK DIAGRAM



Figure 1.

Rev. D
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## AD6645

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## SPECIFICATIONS

## DC SPECIFICATIONS

$A V_{C C}=5 \mathrm{~V}, \mathrm{DV}$ CC $=3.3 \mathrm{~V} ; \mathrm{T}_{\text {MIN }}$ and $\mathrm{T}_{\mathrm{MAX}}$ at rated speed grade, unless otherwise noted.
Table 1.


[^0]
## AD6645

## DIGITAL SPECIFICATIONS

$\mathrm{AV}_{\mathrm{CC}}=5 \mathrm{~V}, \mathrm{DV}_{\mathrm{CC}}=3.3 \mathrm{~V} ; \mathrm{T}_{\text {MIN }}$ and $\mathrm{T}_{\mathrm{MAX}}$ at rated speed grade, unless otherwise noted.
Table 2.

${ }^{1}$ All ac specifications tested by driving ENCODE and ENCODE differentially.
${ }^{2}$ Digital output logic levels: $\mathrm{DV}_{\mathrm{CC}}=3.3 \mathrm{~V}, \mathrm{C}_{\mathrm{LOAD}}=10 \mathrm{pF}$. Capacitive loads $>10 \mathrm{pF}$ degrades performance.

## AC SPECIFICATIONS

All ac specifications tested by driving ENCODE and $\overline{\mathrm{ENCODE}}$ differentially. $\mathrm{AV}_{\mathrm{CC}}=5 \mathrm{~V}, \mathrm{DV} \mathrm{CC}_{\mathrm{CC}}=3.3 \mathrm{~V}$; ENCODE, $\overline{\mathrm{ENCODE}}, \mathrm{T}_{\mathrm{MIN}}$ and $\mathrm{T}_{\mathrm{MAX}}$ at rated speed grade, unless otherwise noted.

Table 3.

| Parameter | Temp | Test <br> Level | $\begin{aligned} & \text { AD6645ASQ-80/ } \\ & \text { AD6645ASV-80 } \end{aligned}$ |  |  | $\begin{gathered} \text { AD6645ASQ-105/ } \\ \text { AD6645ASV-105 } \end{gathered}$ |  |  | Unit | Conditions |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min | Typ | Max | Min | Typ | Max |  |  |
| SNR |  |  |  |  |  |  |  |  |  |  |
| Analog Input @ -1 dBFS | $25^{\circ} \mathrm{C}$ | V |  | 75.0 |  |  | 75.0 |  | dB | At 15.5 MHz |
|  | Full | II | 72.5 | 74.5 |  |  |  |  | dB | At 30.5 MHz |
|  | $25^{\circ} \mathrm{C}$ | II |  |  |  | 72.5 | 74.5 |  | dB | At 37.7 MHz |
|  | Full | II | 72.0 | 73.5 |  | 72.0 | 73.5 |  | dB | At 70.0 MHz |
|  | $25^{\circ} \mathrm{C}$ | V |  | 73.0 |  |  | 73.0 |  | dB | At 150.0 MHz |
|  | $25^{\circ} \mathrm{C}$ | V |  | 72.0 |  |  | 72.0 |  | dB | At 200.0 MHz |
| SINAD |  |  |  |  |  |  |  |  |  |  |
| Analog Input @ - 1 dBFS | $25^{\circ} \mathrm{C}$ | V |  | 75.0 |  |  | 75.0 |  | dB | At 15.5 MHz |
|  | Full | II | 72.5 | 74.5 |  |  |  |  | dB | At 30.5 MHz |
|  | $25^{\circ} \mathrm{C}$ | 1 |  |  |  | 72.5 | 74.5 |  | dB | At 37.7 MHz |
|  | Full | V |  | 73.0 |  |  | 73.0 |  | dB | At 70.0 MHz |
|  | $25^{\circ} \mathrm{C}$ | V |  | 68.5 |  |  | 67.5 |  | dB | At 150.0 MHz |
|  |  |  |  |  |  |  |  |  |  | At 200.0 MHz |
| WORST HARMONIC (SECOND OR THIRD) |  |  |  |  |  |  |  |  |  |  |
| Analog Input @ -1 dBFS | $25^{\circ} \mathrm{C}$ | V |  | 93.0 |  |  | 93.1 |  | dBc | At 15.5 MHz |
|  | Full | II | 85.0 | 93.0 |  |  |  |  | dBC | At 30.5 MHz |
|  | $25^{\circ} \mathrm{C}$ | I |  |  |  | 85.0 | 93.0 |  | dBc | At 37.7 MHz |
|  | Full | V |  | 89.0 |  |  | 87.0 |  | dBc | At 70.0 MHz |
|  | $25^{\circ} \mathrm{C}$ | V |  | 70.0 |  |  | 70.0 |  | dBc | At 150.0 MHz |
|  | $25^{\circ} \mathrm{C}$ | V |  | 63.5 |  |  | 63.5 |  | dBc | At 200.0 MHz |


| Parameter | Temp | Test Level | AD6645ASQ-80/ AD6645ASV-80 |  |  | $\begin{gathered} \hline \text { AD6645ASQ-105/ } \\ \text { AD6645ASV-105 } \end{gathered}$ |  |  | Unit | Conditions |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min | Typ | Max | Min | Typ | Max |  |  |
| WORST HARMONIC (FOURTH OR HIGHER) <br> Analog Input @ -1 dBFS | $\begin{aligned} & 25^{\circ} \mathrm{C} \\ & \text { Full } \\ & 25^{\circ} \mathrm{C} \\ & \text { Full } \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \end{aligned}$ | $\begin{aligned} & \mathrm{V} \\ & \mathrm{II} \\ & \mathrm{I} \\ & \mathrm{~V} \\ & \mathrm{~V} \\ & \mathrm{~V} \\ & \hline \end{aligned}$ | 85.0 | $\begin{aligned} & 96.0 \\ & 95.0 \\ & \\ & 90.0 \\ & 90.0 \\ & 88.0 \\ & \hline \end{aligned}$ |  | 86.0 | $\begin{aligned} & 96.0 \\ & \\ & 95.0 \\ & 90.0 \\ & 90.0 \\ & 88.0 \\ & \hline \end{aligned}$ |  | dBc <br> dBc <br> dBc <br> dBc <br> dBC <br> dBc | At 15.5 MHz At 30.5 MHz At 37.7 MHz At 70.0 MHz At 150.0 MHz At 200.0 MHz |
| TWO-TONE SFDR | $\begin{aligned} & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \mathrm{V} \\ & \mathrm{~V} \\ & \mathrm{~V} \end{aligned}$ |  | $\begin{aligned} & 100 \\ & 100 \end{aligned}$ |  |  | $\begin{aligned} & \hline 98.0 \\ & 98.0 \\ & 98.0 \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \mathrm{dBFS} \\ & \mathrm{dBFS} \\ & \mathrm{dBFS} \\ & \hline \end{aligned}$ | At $30.5 \mathrm{MHz}^{1,2}$ At $55.0 \mathrm{MHz}^{1,3}$ At $70.0 \mathrm{MHz}^{1,4}$ |
| TWO-TONE IMD REJECTION ${ }^{2,3}$ F1, F2 @ -7 dBFS | $25^{\circ} \mathrm{C}$ | V |  | 90 |  |  | 90 |  | dBc |  |
| ANALOG INPUT BANDWIDTH | $25^{\circ} \mathrm{C}$ | V |  | 270 |  |  | 270 |  | MHz |  |

${ }^{1}$ Analog input signal power swept from -10 dBFS to -100 dBFS .
${ }^{2} \mathrm{~F} 1=30.5 \mathrm{MHz}, \mathrm{F} 2=31.5 \mathrm{MHz}$.
${ }^{3} \mathrm{~F} 1=55.25 \mathrm{MHz}, \mathrm{F} 2=56.25 \mathrm{MHz}$.
${ }^{4} \mathrm{~F} 1=69.1 \mathrm{MHz}, \mathrm{F} 2=71.1 \mathrm{MHz}$.

## SWITCHING SPECIFICATIONS

$\mathrm{AV}_{\mathrm{CC}}=5 \mathrm{~V}, \mathrm{DV}_{\mathrm{CC}}=3.3 \mathrm{~V}$; ENCODE, $\overline{\mathrm{ENCODE}}, \mathrm{T}_{\mathrm{MIN}}$ and $\mathrm{T}_{\mathrm{MAX}}$ at rated speed grade, unless otherwise noted.
Table 4.


## AD6645

| Parameter | Symbol | Temp | Test Level | $\begin{aligned} & \text { AD6645ASQ-80/ } \\ & \text { AD6645ASV-80 } \end{aligned}$ |  |  | $\begin{gathered} \text { AD6645ASQ-105/ } \\ \text { AD6645ASV-105 } \end{gathered}$ |  |  | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Min | Typ | Max | Min | Typ | Max |  |
| DATA-READY (DRY4 ${ }^{4}$ /DATA(D13:0),, OVR | th_Dr | Full | V | Note $5^{5}$ |  |  |  |  |  | ns |
| Data-Ready to DATA Delay (Hold Time) |  |  |  |  |  |  | 5.1 | Note | 6.4 |  |
| 50\% Duty Cycle |  | Full | V | 6.6 |  | 7.9 |  | 5.7 |  |  |
| Data-Ready to DATA Delay (Setup Time) | ts_DR | Full <br> Full | V |  | Note $5^{5}$ |  |  | Note |  |  |
| 50\% Duty Cycle |  |  | V | 2.1 | 3.6 | 5.1 | 0.6 | 2.1 | 3.5 | ns |
| APERTURE DELAY | $\mathrm{t}_{\mathrm{A}}$ | $25^{\circ} \mathrm{C}$ | V |  | -500 |  |  | -500 |  | ps |
| APERTURE UNCERTAINTY (JITTER) | $\mathrm{t}_{\mathrm{J}}$ | $25^{\circ} \mathrm{C}$ | V |  | 0.1 |  | 0.1 |  |  | ps rms |

[^1]

Figure 2. Timing Diagram

## ABSOLUTE MAXIMUM RATINGS

Table 5.

| Parameter | Rating |
| :--- | :--- |
| Electrical |  |
| AV cc Voltage | 0 V to 7 V |
| DVcc Voltage | 0 V to 7 V |
| Analog Input Voltage | 0 V to AV cc |
| Analog Input Current | 25 mA |
| Digital Input Voltage | 0 V to AVcc |
| Digital Output Current | 4 mA |
| Environmental |  |
| Operating Temperature Range (Ambient) | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| $\quad$ AD6645-80 | $-10^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| AD6645-105 | $150^{\circ} \mathrm{C}$ |
| Maximum Junction Temperature | $300^{\circ} \mathrm{C}$ |
| Lead Temperature (Soldering, 10 sec) | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Storage Temperature Range (Ambient) |  |

Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## THERMAL RESISTANCE

The heat sink of the AD6645ASVZ, 52-lead TQFP_EP (SV-52-1) package must be soldered to the PCB GND plane to meet thermal specifications.

Table 6. Thermal Characteristics

| Package Type | Rating |
| :--- | :--- |
| 52-Lead TQFP_EP |  |
| $\theta_{\text {JA }}(0 \mathrm{~m} / \mathrm{sec} \text { airflow })^{1,2,3}$ | $23^{\circ} \mathrm{C} / \mathrm{W}$, soldered heat sink |
| $\theta_{\text {JMA }}(1.0 \mathrm{~m} / \mathrm{sec} \text { airflow })^{2,3,4,5}$ | $17^{\circ} \mathrm{C} / \mathrm{W}$, soldered heat sink |
| $\theta_{\mathrm{Jc}} \mathrm{c}^{6,7}$ | $2^{\circ} \mathrm{C} / \mathrm{W}$, soldered heat sink |
| 52 -Lead LQFP_PQ4 |  |
| $\theta_{\text {JA }}(0 \mathrm{~m} / \mathrm{sec} \text { airflow })^{1,2,3}$ | $30^{\circ} \mathrm{C} / \mathrm{W}$, unsoldered heat sink |
| $\theta_{\text {JMA }}\left(1.0 \mathrm{~m} /\right.$ sec airflow ${ }^{2,3,4,5}$ | $24^{\circ} \mathrm{C} / \mathrm{W}$, unsoldered heat sink |
| $\theta_{\text {JA }}(0 \mathrm{~m} / \mathrm{sec} \text { airflow })^{1,2,3}$ | $23^{\circ} \mathrm{C} / \mathrm{W}$, soldered heat sink |
| $\theta_{\text {JMA }}(1.0 \mathrm{~m} / \text { sec airflow })^{2,3,4,5}$ | $17^{\circ} \mathrm{C} / \mathrm{W}$, soldered heat sink |
| $\theta_{\mathrm{JC}}{ }^{6,7}$ | $2^{\circ} \mathrm{C} / \mathrm{W}$ |

[^2]Values of $\theta_{\mathrm{JA}}$ are provided for package comparison and PCB design considerations. $\theta_{\text {JA }}$ can be used for a first-order approximation of $\mathrm{T}_{J}$ by the equation

$$
T_{J}=T_{A}+\left(\theta_{J A} \times P D\right)
$$

where:
$T_{A}$ is the ambient temperature ( ${ }^{\circ} \mathrm{C}$ ).
$P D$ is the power dissipation (W).

## EXPLANATION OF TEST LEVELS

I. $100 \%$ production tested.
II. $100 \%$ production tested at $25^{\circ} \mathrm{C}$ and guaranteed by design and characterization at temperature extremes.
III. Sample tested only.
IV. Parameter is guaranteed by design and characterization testing.
V. Parameter is a typical value only.

## ESD CAUTION

|  | ESD (electrostatic discharge) sensitive device. <br> Charged devices and circuit boards can discharge <br> without detection. Although this product features <br> patented or proprietary protection circuitry, damage <br> may occur on devices subjected to high energy ESD. <br> Therefore, proper ESD precautions should be taken to <br> avoid performance degradation or loss of functionality. |
| :--- | :--- |

## AD6645

## PIN CONFIGURATION AND FUNCTION DESCRIPTIONS



NOTES

1. DNC = DO NOT CONNECT
2. EXPOSED PAD. CONNECT THE EXPOSED PAD TO GND.

Figure 3. Pin Configuration

Table 7. Pin Function Descriptions

| Pin Number | Mnemonic | Description |
| :---: | :---: | :---: |
| 1,33,43 | DV ${ }_{\text {cc }}$ | 3.3 V Power Supply (Digital) Output Stage Only. |
| $\begin{aligned} & 2,4,7,10,13,15,17,19,21,23,25, \\ & 27,29,34,42 \end{aligned}$ | GND | Ground. |
| 3 | VREF | 2.4V Reference. Bypass to ground with a $0.1 \mu \mathrm{~F}$ microwave chip capacitor. |
| 5 | ENCODE | Encode Input. Conversion initiated on rising edge. |
| 6 | $\overline{\text { ENCODE }}$ | Complement of $\overline{\text { ENCODE, Differential Input. }}$ |
| 8, 9, 14, 16, 18, 22, 26, 28, 30 | AV ${ }_{\text {cc }}$ | 5 V Analog Power Supply. |
| 11 | AIN | Analog Input. |
| 12 | $\overline{\text { AIN }}$ | Complement of AIN, Differential Analog Input. |
| 20 | C1 | Internal Voltage Reference. Bypass to ground with a $0.1 \mu \mathrm{~F}$ chip capacitor. |
| 24 | C2 | Internal Voltage Reference. Bypass to ground with a $0.1 \mu \mathrm{~F}$ chip capacitor. |
| 31 | DNC | Do not connect this pin. |
| 32 | OVR | Overrange Bit. A logic level high indicates analog input exceeds $\pm$ FS. |
| 35 | DMID | Output Data Voltage Midpoint. Approximately equal to ( $\mathrm{VV}_{\mathrm{cc}}$ )/2. |
| 36 | D0 (LSB) | Digital Output Bit (Least Significant Bit); Twos Complement. |
| 37 to 41, 44 to 50 | D1 to D5, D6 to D12 | Digital Output Bits in Twos Complement. |
| 51 | D13 (MSB) | Digital Output Bit (Most Significant Bit); Twos Complement. |
| 52 | DRY | Data-Ready Output. |
| 53 (EPAD) | Exposed Paddle (EPAD) | Exposed Pad. Connect the exposed pad to GND. |

## TYPICAL PERFORMANCE CHARACTERISTICS



Figure 4. Single Tone @ 2.2 MHz


Figure 5. Single Tone @ 15.5 MHz


Figure 6. Single Tone @ 29.5 MHz


Figure 7. Single Tone @ 69.1 MHz


Figure 8. Single Tone @ 150 MHz


Figure 9. Single Tone @ 200 MHz

## AD6645



Figure 10. Signal-to-Noise Ratio (SNR) vs. Frequency


Figure 11. Worst-Case Harmonics vs. Analog Input Frequency


Figure 12. Signal-to-Noise Ratio (SNR) vs. Analog Frequency (IF)


Figure 13. Harmonics vs. Analog Frequency (IF)


Figure 14. Single-Tone SFDR @ 30.5 MHz


Figure 15. Single-Tone SFDR @ 69.1 MHz


Figure 16. Two-Tone SFDR @ 30.5 MHz and 31.5 MHz


Figure 17. Two-Tone SFDR @ 30.5 MHz and 31.5 MHz


Figure 18. SNR, Worst-Case Spurious vs. Encode @ 2.2 MHz


Figure 19. Two-Tone SFDR @ 55.25 MHz and 56.25 MHz


Figure 20. Two-Tone SFDR @ 55.25 MHz and 56.25 MHz


Figure 21. SNR, Worst-Case Spurious vs. Encode @ 69.1 MHz

## AD6645



Figure 22.1 M Sample FFT Without Dither


Figure 23. SFDR Without Dither


Figure 24. Single Tone @ 69.1 MHz, Encode = 76.8 MSPS


Figure 25.1 M Sample FFT with Dither


Figure 26. SFDR with Dither


Figure 27. W-CDMA Tone @ 69.1 MHz, Encode = 76.8 MSPS


Figure 28. Two W-CDMA Carriers @ 59.6 MHz, Encode = 76.8 MSPS


Figure 29. Four W-CDMA Carriers @ 46.08 MHz , Encode $=61.44 \mathrm{MSPS}$


Figure 30. W-CDMA Tone @ 140 MHz , Encode $=76.8$ MSPS


Figure 31. W-CDMA Tone @ 190 MHz, Encode = 61.44 MSPS

## AD6645

## EQUIVALENT CIRCUITS



## TERMINOLOGY

## Analog Bandwidth

The analog input frequency at which the spectral power of the fundamental frequency (as determined by the FFT analysis) is reduced by 3 dB .

## Aperture Delay

The delay between the $50 \%$ point of the rising edge of the encode command and the instant at which the analog input is sampled.

## Aperture Uncertainty (Jitter)

The sample-to-sample variation in aperture delay.

## Differential Analog Input Resistance, Differential Analog

 Input Capacitance, and Differential Analog Input Impedance The real and complex impedances measured at each analog input port. The resistance is measured statically and the capacitance and differential input impedances are measured with a network analyzer.
## Differential Analog Input Voltage Range

The peak-to-peak differential voltage that must be applied to the converter to generate a full-scale response. The peak differential voltage is computed by observing the voltage on a single pin and subtracting the voltage from the other pin, which is $180^{\circ}$ out of phase. The peak-to-peak differential is computed by rotating the inputs' phase $180^{\circ}$ and taking the peak measurement again. The difference is then computed between both peak measurements.

## Differential Nonlinearity

The deviation of any code width from an ideal 1 LSB step.

## Encode Pulse Width/Duty Cycle

Pulse width high is the minimum amount of time that the encode pulse should be left in a high state to achieve rated performance; pulse width low is the minimum time that the encode pulse should be left in a low state. See timing implications of changing $\mathrm{t}_{\mathrm{ENCH}}$ in Table 4. At a given clock rate, these specifications define an acceptable encode duty cycle.

## Full-Scale Input Power

The full-scale input power is expressed in dBm and can be calculated by using the following equation:

$$
\text { Power }_{\text {Full }- \text { Scale }}=10 \log \left[\frac{\frac{V^{2} \text { Full }- \text { Scalerms }}{|Z|_{\text {Input }}}}{0.001}\right]
$$

## Harmonic Distortion, Second

The ratio of the rms signal amplitude to the rms value of the second harmonic component, reported in dBc.

## Harmonic Distortion, Third

The ratio of the rms signal amplitude to the rms value of the third harmonic component, reported in dBc .

## Integral Nonlinearity

The deviation of the transfer function from a reference line measured in fractions of 1 LSB using a best straight line determined by a least square curve fit.

## Maximum Conversion Rate

The encode rate at which parametric testing is performed.

## Minimum Conversion Rate

The encode rate at which the SNR of the lowest analog signal frequency drops by no more than 3 dB below the guaranteed limit.
Noise (for Any Range Within the ADC)

$$
V_{\text {NOISE }}=\sqrt{|Z| \times 0.001 \times 10\left(\frac{F S_{d B m}-S N R_{d B c}-\text { Signal }_{d B F S}}{10}\right)}
$$

where:
$Z$ is the input impedance.
$F S$ is the full scale of the device for the frequency in question.
$S N R$ is the value for the particular input level.
Signal is the signal level within the ADC reported in dB below full scale. This value includes both thermal noise and quantization noise.

Output Propagation Delay
The delay between a differential crossing of ENCODE and
$\overline{\text { ENCODE }}$ and the time when all output data bits are within valid logic levels.

## Power Supply Rejection Ratio (PSSR)

The ratio of a change in input offset voltage to a change in power supply voltage.

## Power Supply Rise Time

The time from when the dc supply is initiated until the supply output reaches the minimum specified operating voltage for the ADC . The dc level is measured at the supply pin(s) of the ADC.

## Signal-to-Noise-and-Distortion (SINAD)

The ratio of the rms signal amplitude (set at 1 dB below full scale) to the rms value of the sum of all other spectral components, including harmonics, but excluding dc.

## Signal-to-Noise Ratio (Without Harmonics)

The ratio of the rms signal amplitude (set at 1 dB below full scale) to the rms value of the sum of all other spectral components, excluding the first five harmonics and dc.

## AD6645

## Spurious-Free Dynamic Range (SFDR)

The ratio of the rms signal amplitude to the rms value of the peak spurious spectral component. The peak spurious component may or may not be a harmonic. May be reported in dBc (that is, degrades as signal level is lowered) or dBFS (always related back to converter full scale).

## Two-Tone Intermodulation Distortion Rejection

The ratio of the rms value of either input tone to the rms value of the worst third-order intermodulation product, reported in dBc .

## Two-Tone SFDR

The ratio of the rms value of either input tone to the rms value of the peak spurious component. The peak spurious component may or may not be an IMD product, and may be reported in dBc (that is, degrades as signal level is lowered) or in dBFS (always related back to converter full scale).

## Worst Other Spur

The ratio of the rms signal amplitude to the rms value of the worst spurious component (excluding the second and third harmonics), reported in dBc .

## THEORY OF OPERATION

The AD6645 ADC employs a three-stage subrange architecture. This design approach achieves the required accuracy and speed while maintaining low power and small die size.
As shown in the functional block diagram (see Figure 1), the AD6645 has complementary analog input pins, AIN and AIN. Each analog input is centered at 2.4 V and should swing $\pm 0.55 \mathrm{~V}$ around this reference (see Figure 32). Because AIN and AIN are $180^{\circ}$ out of phase, the differential analog input signal is 2.2 V p-p.
Both analog inputs are buffered prior to the first track-and-hold, TH1. The high state of the encode pulse places TH1 in hold mode. The held value of TH1 is applied to the input of a 5 -bit coarse ADC1. The digital output of $\mathrm{ADC1}$ drives a 5 -bit digital-to-analog converter, DAC1. DAC1 requires 14 bits of precision that is achieved through laser trimming. The output of DAC1 is subtracted from the delayed analog signal at the input of TH3 to generate a first residue signal. TH2 provides an analog pipeline delay to compensate for the digital delay of ADC1.
The first residual signal is applied to a second conversion stage consisting of a 5-bit ADC2, a 5-bit DAC2, and a pipeline TH4. The second DAC requires 10 bits of precision, which is met by the process with no trim. The input to TH5 is a second residual signal generated by subtracting the quantized output of DAC2 from the first residual signal held by TH4. TH5 drives a final 6-bit ADC3.

The digital outputs from $\mathrm{ADC} 1, \mathrm{ADC} 2$, and ADC 3 are added together and corrected in the digital error correction logic to generate the final output data. The result is a 14 -bit parallel digital CMOS-compatible word, coded as twos complement.

## APPLYING THE AD6645

## Encoding the AD6645

The AD6645 encode signal must be a high quality, extremely low phase noise source to prevent degradation of performance. Maintaining 14-bit accuracy places a premium on encode clock phase noise. SNR performance can easily degrade by 3 dB to 4 dB with 70 MHz analog input signals when using a high jitter clock source. See the AN-501 application note, Aperture Uncertainty and ADC System Performance, for complete details.
For optimum performance, the AD6645 must be clocked differentially. The encode signal is usually ac-coupled into the ENCODE and $\overline{\text { ENCODE }}$ pins via a transformer or capacitors. These pins are biased internally and require no additional bias.
Figure 38 shows one preferred method for clocking the AD6645. The clock source (low jitter) is converted from single-ended to differential using an RF transformer. The back-to-back Schottky diodes across the transformer secondary limit excessive amplitude swings from the clock into the AD6645 to approximately 0.8 V p-p differential. This helps to prevent the large voltage swings of the clock from feeding through to other portions of the AD6645 and limits the noise presented to the encode inputs.


Figure 38. Crystal Clock Oscillator, Differential Encode
If a low jitter clock is available, another option is to ac-couple a differential ECL/PECL signal to the encode input pins, as shown in Figure 39. The MC100EL16 (or same family) from ON Semiconductor offers excellent jitter performance.


Figure 39. Differential ECL for Encode

## Driving the Analog Inputs

As with most new high speed, high dynamic range ADCs, the analog input to the AD6645 is differential. Differential inputs improve on-chip performance as signals are processed through attenuation and gain stages. Most of the improvement is a result of differential analog stages having high rejection of even-order harmonics. There are also benefits at the PCB level. First, differential inputs have high common-mode rejection of stray signals, such as ground and power noise. Second, they provide good rejection of common-mode signals, such as local oscillator feedthrough.
The AD6645 analog input voltage range is offset from ground by 2.4 V. Each analog input connects through a $500 \Omega$ resistor to the 2.4 V bias voltage and to the input of a differential buffer (see Figure 32). The resistor network on the input properly biases the followers for maximum linearity and range. Therefore, the analog source driving the AD6645 should be ac-coupled to the input pins. Because the differential input impedance of the AD6645 is $1 \mathrm{k} \Omega$, the analog input power requirement is only -2 dBm , simplifying the driver amplifier in many cases. To take full advantage of this high input impedance, a 20:1 RF transformer is required. This is a large ratio and can result in unsatisfactory performance. In this case, a lower step-up ratio can be used. The recommended method for driving the differential analog input of the AD6645 is to use a 4:1 RF transformer. For example, if $\mathrm{R}_{\mathrm{T}}$ is set to $60.4 \Omega$ and $\mathrm{R}_{\mathrm{S}}$ is set to $25 \Omega$, along with a $4: 1$ impedance ratio transformer, the input would match to a $50 \Omega$ source with a full-scale drive of 4.8 dBm . Series resistors ( $\mathrm{R}_{\mathrm{s}}$ ) on the secondary side of the transformer should be used to isolate the transformer from the A/D.

## AD6645

This limits the amount of dynamic current from the A/D flowing back into the secondary of the transformer. The $50 \Omega$ impedance matching can also be incorporated on the secondary side of the transformer, as shown in the evaluation board schematic (see Figure 43).


Figure 40. Transformer-Coupled Analog Input Circuit
In applications where dc coupling is required, a differential output op amp, such as the AD8138, can be used to drive the AD6645 (see Figure 41). The AD8138 op amp provides single-ended-to-differential conversion, which reduces overall system cost and minimizes layout requirements.


Figure 41. DC-Coupled Analog Input Circuit

## Power Supplies

Care should be taken when selecting a power source. The use of linear dc supplies with rise times of $<45 \mathrm{~ms}$ is highly recommended. Switching supplies tend to have radiated components that can be received by the AD6645. Decouple each of the power supply pins as close to the package as possible using $0.1 \mu \mathrm{~F}$ chip capacitors.
The AD6645 has separate digital and analog power supply pins. The analog supplies are $A V_{C C}$ and the digital supply pins are DV cc. Although analog and digital supplies can be tied together, the best performance is achieved when the supplies are separate because the fast digital output swings can couple switching currents back into the analog supplies. Note that $\mathrm{AV}_{\mathrm{CC}}$ must be held within $5 \%$ of 5 V . The AD6645 is specified for $\mathrm{DV}_{\mathrm{CC}}=3.3 \mathrm{~V}$, a common supply for digital ASICs.

## Digital Outputs

Care must be taken when designing the data receivers for the AD6645. It is recommended that the digital outputs drive a series resistor followed by a gate, such as the 74LCX574.

To minimize capacitive loading, there should be only one gate on each output pin. An example of this is shown in the evaluation board schematic of Figure 43. The digital outputs of the AD6645 have a constant output slew rate of $1 \mathrm{~V} / \mathrm{ns}$. A typical CMOS gate combined with a PCB trace have a load of approximately 10 pF . Therefore, as each bit switches, $10 \mathrm{~mA}(10 \mathrm{pF} \times 1 \mathrm{~V} \div 1 \mathrm{~ns})$ of dynamic current per bit flow in or out of the device. A full-scale transition can cause up to 140 mA ( 14 bits $\times 10 \mathrm{~mA} /$ bit ) of current to flow through the output stages. Place the series resistors as close to the AD6645 as possible to limit the amount of current that can flow into the output stage. These switching currents are confined between ground and DV ${ }_{\mathrm{cc}}$. Standard TTL gates should be avoided because they can add appreciably to the dynamic switching currents of the AD6645. Note that extra capacitive loading increases output timing and invalidates timing specifications. Digital output timing is guaranteed for output loads up to 10 pF . Digital output states for given analog input levels are shown in Table 8.

## Grounding

For optimum performance, it is highly recommended that a common ground be used between the analog and digital power planes. The primary concern with splitting grounds is that dynamic currents may be forced to travel significant distances in the system before recombining back at the common source ground. This can result in a large, undesirable ground loop. The most common place for this to occur is on the digital outputs of the ADC. Ground loops can contribute to digital noise being coupled back onto the ADC front end. This can manifest itself as either harmonic spurs, or very high-order spurious products that can cause excessive spikes on the noise floor. This noise coupling is less likely to occur at lower clock speeds because the digital noise has more time to settle between samples. In general, splitting the analog and digital grounds can frequently contribute to undesirable EMI-RFI and should, therefore, be avoided.
Conversely, if not properly implemented, common grounding can actually impose additional noise issues because the digital ground currents ride on top of the analog ground currents in close proximity to the ADC input. To further minimize the potential for noise coupling, it is highly recommended that multiple ground return traces/vias be placed such that the digital output currents do not flow back toward the analog front end but are routed quickly away from the ADC. This does not require a split in the ground plane and can be accomplished by simply placing substantial ground connections directly back to the supply at a point between the analog front end and the digital outputs. In addition, the judicious use of ceramic chip capacitors between the power supply and ground planes helps to suppress digital noise. The layout should incorporate enough bulk capacitance to supply the peak current requirements during switching periods.

## LAYOUT INFORMATION

The schematic of the evaluation board (see Figure 43) represents a typical implementation of the AD6645. A multilayer board is recommended to achieve best results. It is highly recommended that high quality, ceramic chip capacitors be used to decouple each supply pin to ground directly at the device. The pinout of the AD6645 facilitates ease of use in the implementation of high frequency, high resolution design practices. All of the digital outputs are segregated to two sides of the chip, with the inputs on the opposite side for isolation purposes.

Care should be taken when routing the digital output traces. To prevent coupling through the digital outputs into the analog portion of the AD6645, minimal capacitive loading should be placed on these outputs. It is recommended that a fanout of only one gate should be used for all AD6645 digital outputs.
The layout of the encode circuit is equally critical. Any noise received on this circuitry results in corruption in the digitization process and lower overall performance. The encode clock must be isolated from the digital outputs and the analog inputs.

Table 8. Twos Complement Output Coding

| AIN Level | $\overline{\text { AIN }}$ Level | Output State | Output Code |
| :--- | :--- | :--- | :--- |
| VREF +0.55 V | VREF -0.55 V | Positive FS | 01111111111111 |
| VREF | VREF | Midscale | $00 \ldots 0 / 11 \ldots 1$ |
| VREF -0.55 V | VREF +0.55 V | Negative FS | 10000000000000 |

## JITTER CONSIDERATIONS

The SNR for an ADC can be predicted. When normalized to ADC codes, the following equation accurately predicts the SNR based on three terms: jitter, average DNL error, and thermal noise. Each of these terms contributes to the noise within the converter.
$S N R=1.76-$
$20 \log \left[\left(2 \pi \times f_{\text {ANALOG }} \times t_{j r m s}\right)^{2}+\left(\frac{1+\varepsilon}{2^{n}}\right)^{2}+\left(\frac{2 \times \sqrt{2} \times V_{\text {NOISE rms }}}{2^{n}}\right)^{2}\right]^{1 / 2}$ where:
$f_{A N A L O G}$ is the analog input frequency.
$t_{j r m s}$ is the rms jitter of the encode (rms sum of encode source and internal encode circuitry).
$\varepsilon$ is the average DNL of the ADC (typically 0.41 LSB ).
$n$ is the number of bits in the ADC.
$V_{\text {NoISE rms }}$ is the voltage rms thermal noise that refers to the analog input of the ADC (typically 0.9 LSB rms).
For a 14-bit ADC, such as the AD6645, aperture jitter can greatly affect the SNR performance as the analog frequency is increased. Figure 42 shows a family of curves that demonstrate the expected SNR performance of the AD6645 as jitter increases. The chart is derived from the preceding equation.
For a complete discussion of aperture jitter, see the AN-756 application note, Sampled Systems and the Effects of Clock Phase Noise and Jitter. The AN-756 application note can be found on www.analog.com.


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Table 9. AD6645/PCB Bill of Materials

| Quantity 80 MSPS | Quantity 105 MSPS | Reference ID | Description | Manufacturer | Supplier Part No. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1 | PCB | Printed circuit board, AD6645 engineering evaluation board | PCSM | 6645EE01D REV D |
| 4 | 4 | C1, C2, C31, C38 | Capacitor, tantalum, SMT BCAPTAJC, $10 \mu \mathrm{~F}, 16 \mathrm{~V}, 10 \%$ | Kemet | T491C106K016AS |
| 8 | 8 | $\begin{aligned} & \text { C3, C7 to C10, C16, } \\ & \text { C30 }{ }^{1} \text {, C32 } \end{aligned}$ | Capacitor, ceramic, SMT 0508, $0.1 \mu \mathrm{~F}, 16 \mathrm{~V}, 10 \%$ | Presidio Components | 0508X7R104K16VP3 |
| 9 | 9 | $\begin{aligned} & \text { C4, C15, C22 to } \\ & \text { C26, C29, (C33 }{ }^{2,3}, \\ & (\mathrm{C} 34)^{2,3}, \mathrm{C} 39 \end{aligned}$ | Capacitor, ceramic, SMT 0805, $0.1 \mu \mathrm{~F}, 25 \mathrm{~V}, 10 \%$ | Panasonic | ECJ-2VB1E104K |
| 0 | 0 | (C5, C6) ${ }^{2,3}$ | Capacitor, ceramic, SMT 0805, $0.01 \mu \mathrm{~F}, 50 \mathrm{~V}, 10 \%$ | Panasonic | ECJ-2YB1H103K |
| 10 | 10 | $\begin{aligned} & \text { C11 to C14, } \\ & \text { C17 to C21, C40 } \end{aligned}$ | Capacitor, ceramic, SMT 0508, $0.01 \mu \mathrm{~F}, 50 \mathrm{~V}, 0.2 \%$ | Presidio Components | 0508X7R103M2P3 |
| 0 | 0 | (C27, C28) ${ }^{2}$ | Capacitor, ceramic, SMT 0805, limits amp bandwidth as warranted |  |  |
| 1 | 1 | CR1 ${ }^{3}$ | Diode, dual Schottky HSMS2812, SOT-23, $30 \mathrm{~V}, 20 \mathrm{~mA}$ | Panasonic | MA716-(TX) |
| 1 | 1 | E1 | Install jumper wire (across OPT_LAT and BUFLAT) |  |  |
| 5 | 5 | F1 to F5 | EMI suppression ferrite chip, SMT 0805 | Steward | HZ0805E601R-00 |
| 1 | 1 | J1 | Header, 6-pin, pin strip, 5 mm pitch | Wieland | Z5.530.0625.0 |
| 1 | 1 | J1 | Pin strip, 6-pin, 5 mm pitch | Wieland | 25.602.2653.0 |
| 1 | 1 | J2 | Header, 40-pin, male, right angle | Samtec | TSW-120-08-T-D-RA |
| 2 | 2 | (J3) ${ }^{2}$, J4, J5 | Connector, gold, female, coax., SMA, vertical | Johnson Components | 142-0701-201 |
| 1 | 1 | L1 | Inductor, SMT, 1008-ct package, 4.7 nH | Coilcraft | 1008CT-040X-J |
| 0 | 0 | (R1) ${ }^{2,3}$ | Resistor, thick film, SMT 0402, $100 \Omega$, 1/16 W, 1\% | Panasonic | ERJ-2RKF1000 |
| 0 | 0 | (R2) ${ }^{2}$ | Resistor, thick film, SMT 1206, $60.4 \Omega$, 1/4 W, 1\% | Panasonic | ERJ-8ENF60R4V |
| 2 | 2 | $\begin{aligned} & (\text { R3 to R5 })^{1,2},(\text { R8 })^{1,2}, \\ & \text { R9, R10 } \end{aligned}$ | Resistor, thick film, SMT 0805, $500 \Omega$, 1/8 W, 1\% | Panasonic | ERJ-6ENF4990V |
| 2 | 2 | R6, R7 | Resistor, thick film, SMT 0805, $25.5 \Omega$, 1/8 W, 1\% | Panasonic | ERJ-6ENF25R5V |
| 0 | 0 | $(\mathrm{R} 11)^{2,3},(\mathrm{R} 13)^{2,3}$ | Resistor, thick film, SMT 0805, $66.5 \Omega$, 1/8 W, 1\% | Panasonic | ERJ-6ENF66R5V |
| 0 | 0 | $(\mathrm{R} 12)^{2,3},(\mathrm{R} 14)^{2,3}$ | Resistor, thick film, SMT 0805, $100 \Omega$, 1/8W, 1\% | Panasonic | ERJ-6ENF1000V |
| 1 | 1 | R15 ${ }^{1}$ | Resistor, thick film, SMT 0402, $178 \Omega$, 1/16 W, 1\% | Panasonic | ERJ-2RKF1780X |
| 1 | 1 | R35 | Resistor, thick film, SMT 0805, $49.9 \Omega$, 1/8 W, 1\% | Panasonic | ERJ-6ENF49R9V |
| 4 | 4 | RN1 to RN4 | Resistor array, SMT 0402; $100 \Omega$; 8 ISO RES.,1/4 W; 5\% | Panasonic | EXB2HV101JV |
| 2 | 2 | T2 ${ }^{3}$, $3^{1}$ | $\begin{aligned} & \text { Transformer, ADT4-1WT, CD542, } \\ & 2 \mathrm{MHz} \text { to } 775 \mathrm{MHz} \end{aligned}$ | Mini-Circuits | ADT4-1WT |
| 1 | 0 | U1 | IC, 14-bit, 80 MSPS ADC | Analog Devices | AD6645ASQ/ASV-80 |
| 0 | 1 | U1 | IC, 14-bit, 105 MSPS ADC | Analog Devices | AD6645ASQ/ASV-105 |
| 2 | 2 | U2, U7 | IC, SOIC-20, Octal D-type flip-flop | Fairchild | 74LCX574WM |
| 0 | 0 | (U3) ${ }^{1,2}$ | IC, SOIC-8, low distortion differential ADC driver | Analog Devices | AD8138AR |
| 2 | 2 | U4, U6 | IC, SOT-23, tiny logic UHS 2 input OR gate | Fairchild | NC7SZ32 |


| Quantity <br> 80 MSPS | Quantity <br> 105 MSPS | Reference ID | Description | Manufacturer | Supplier Part No. |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 0 | 0 | $(U 8)^{2,3}$ | IC, SOIC-8, differential receiver | Motorola | MC100LVEL16 |
| 1 | 0 | Y1 | Clock oscillator, 80 MHz | CTS Reeves | MXO45-80 |
| 4 | 4 | Y1 | Pin sockets, closed end | AMP/Tyco Electronics | $5-330808-3$ |
| 4 | 4 |  | Circuit board support | Richco, Inc. | CBSB-14-01 |

${ }^{1}$ AC-coupled AIN is standard: R3, R4, R5, R8, and U3 are not installed. If dc-coupled AIN is required, C30, R15, and T3 are not installed.
${ }^{2}$ Reference designators in parentheses are not installed on standard units.
${ }^{3}$ AC-coupled encode is standard: C5, C6, C33, C34, R1, R11 to R14, and U8 are not installed. If PECL encode is required, CR1 and T2 are not installed.


Figure 43. Evaluation Board Schematic


Figure 44. Top Signal Level


Figure 45. 5.0 V Plane Layer 3 and 3.3 V Plane Layer 4


Figure 46. Ground Plane Layer 2 and Ground Plane Layer 5


Figure 47. Bottom Signal Layer

## AD6645

## OUTLINE DIMENSIONS



Figure 49. 52-Lead Thin Quad Flat Package, Exposed Pad [TQFP_EP]
(SV-52-1)
Dimensions shown in millimeters
ORDERING GUIDE

| Model | Temperature Range | Package Description | Package Option |
| :---: | :---: | :---: | :---: |
| AD6645ASQ-80 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 52-Lead Low Profile Quad Flat Package, PowerQuad (LQFP_PQ4) | SQ-52-1 |
| AD6645ASQZ-80 ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 52-Lead Low Profile Quad Flat Package, PowerQuad (LQFP_PQ4) | SQ-52-1 |
| AD6645ASVZ-80 ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 52-Lead Thin Quad Flat Package, Exposed Pad [TQFP_EP] | SV-52-1 |
| AD6645ASQ-105 | $-10^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 52-Lead Low Profile Quad Flat Package, PowerQuad (LQFP_PQ4) | SQ-52-1 |
| AD6645ASQZ-1051 | $-10^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 52-Lead Low Profile Quad Flat Package, PowerQuad (LQFP_PQ4) | SQ-52-1 |
| AD6645ASVZ-105 ${ }^{1}$ | $-10^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 52-Lead Thin Quad Flat Package, Exposed Pad [TQFP_EP] | SV-52-1 |
| AD6645-80/PCBZ ${ }^{1}$ |  | Evaluation Board |  |
| AD6645-105/PCBZ ${ }^{1}$ |  | Evaluation Board |  |

${ }^{1} Z=$ RoHS Compliant Part.


[^0]:    ${ }^{1}$ VREF is provided for setting the common-mode offset of a differential amplifier, such as the AD8138, when a dc-coupled analog input is required. VREF should be buffered if used to drive additional circuit functions.
    ${ }^{2}$ Specified for dc supplies with linear rise time characteristics.

[^1]:    ${ }^{1}$ Several timing parameters are a function of $\mathrm{t}_{\mathrm{ENC}}$ and $\mathrm{t}_{\text {ENCH }}$.
    ${ }^{2}$ Several timing parameters are a function of tencl and tench.
    ${ }^{3}$ ENCODE TO DATA Delay (Hold Time) is the absolute minimum propagation delay through the ADC, $\mathrm{t}_{\mathrm{E} \text { RL }}=\mathrm{t}_{\mathrm{H}_{-} \mathrm{E}}$.
    ${ }^{4}$ DRY is an inverted and delayed version of the encode clock. Any change in the duty cycle of the clock will correspondingly change the duty cycle of DRY.
    ${ }^{5}$ Data-ready to DATA Delay ( $t_{H_{-} \text {Rr }}$ and $\mathrm{t}_{S_{-} \mathrm{DR}}$ ) is calculated relative to rated speed grade and is dependent on $\mathrm{t}_{\text {ENC }}$ and duty cycle.

[^2]:    ${ }^{1}$ Per JEDEC JESD51-2 (heat sink soldered to PCB).
    ${ }^{2}$ 2S2P JEDEC test board.
    ${ }^{3}$ Values of $\theta_{\mathrm{JA}}$ are provided for package comparison and PCB design considerations.
    ${ }^{4}$ Per JEDEC JESD51-6 (heat sink soldered to PCB).
    ${ }^{5}$ Airflow increases heat dissipation, effectively reducing $\theta_{\mathrm{JA}}$. Furthermore, the more metal that is directly in contact with the package leads from metal traces, throughholes, ground, and power planes, the more $\theta_{\mathrm{JA}}$ is reduced.
    ${ }^{6}$ Per MIL-STD-883, Method 1012.1.
    ${ }^{7}$ Values of $\theta$ ィ are provided for package comparison and PCB design considerations when an external heat sink is required.

